Feedback control of NMR systems: a control-theoretic perspective – PART 2 –

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This lecture

- Model for a 2 spin 1/2 system
- State feedback control for a weakly coupled system
- Tracking an Hamiltonian different from the real one: suppression of unwanted weak couplings
- design open-loop controls based on "feedback on the simulator"
- examples on 3 and 4 spins

Product operators basis

• (rescaled) identity + Pauli matrices

$$\lambda_0 = \frac{1}{\sqrt{2}} \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}, \qquad \lambda_j = \frac{1}{\sqrt{2}} \sigma_j, \qquad j = 1, 2, 3$$

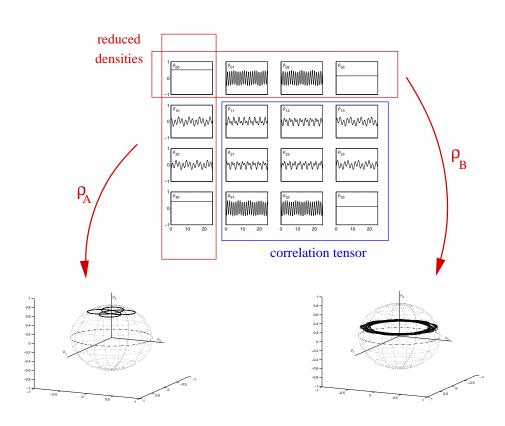
• product operators $\Lambda_{jk} = \lambda_j \otimes \lambda_k$, $j, k = 0, \dots, 3$:

- **O** 0 spin operators Λ_{00}
- 1 spin operators Λ_{01} , Λ_{02} , Λ_{03} , Λ_{10} , Λ_{20} , Λ_{30}
- 2 spin operators Λ_{11} , Λ_{12} , Λ_{13} , Λ_{21} , Λ_{22} , Λ_{23} , Λ_{31} , Λ_{32} , Λ_{33}
- basis for

o density $\rho = \sum_{j, k=0}^{3} \varrho^{jk} \Lambda_{jk}$ where $\varrho^{jk} = \operatorname{tr} (\rho \Lambda_{jk})$ **o** Hamiltonian $H = h^{jl} \Lambda_{jk}$

Two spin $\frac{1}{2}$ **: density operator as a tensor**

• state tensor ρ : 16 components • $\rho^{00} = \operatorname{tr} (\rho \Lambda_{00}) = \operatorname{const} \Longrightarrow \operatorname{trace \ component \ of \ \rho}$ • $\{ \rho^{10}, \ \rho^{20}, \ \rho^{30} \}$ reduced density ρ_A • $\{ \rho^{01}, \ \rho^{02}, \ \rho^{03} \}$ reduced density ρ_B • $\{ \rho^{11}, \ \rho^{12}, \dots, \rho^{33} \}$ 2-body correlations



Two spin $\frac{1}{2}$ **: density operator as a tensor**

- structure of the space of tensors ϱ^{jk}
 - ρ^{jk} = elements of a "Liouville space"
 - **O** $\boldsymbol{\varrho} = \{ \ \varrho^{jk} \ \}$ = Stokes tensor
 - $\bullet \ \varrho^{jk} \in \mathbb{R} \Longrightarrow \boldsymbol{\varrho} \in \mathcal{S} \subset \mathbb{S}^{14}$
 - o 15 components
 - 6 independent degrees of freedom for pseudopure states
 - $o \implies$ structure of S includes several constraints (independent from the degree of purity)
 - $\mathbf{O} \Longrightarrow$ structure of \mathcal{S} is complicated to "visualize"

Two spin $\frac{1}{2}$ **: density operator as a tensor**

• $tr\Lambda_{jk}\Lambda_{lm} = \delta_{jk}\delta_{lm} \Longrightarrow \Lambda_{jk}$ form a complete orthonormal set

• trace norm \implies Euclidean norm in ϱ^{jk} -space

$$\operatorname{tr}\left(\rho^{2}\right) = \operatorname{tr}\left(\left(\varrho^{jk}\Lambda_{jk}\right)^{2}\right) = \sum_{j,k=0}^{3} \left(\varrho^{jk}\right)^{2} = \left\|\varrho\right\|^{2} \leqslant 1$$

• inner product

$$\operatorname{tr}(\rho_1\rho_2) = \langle\!\langle \boldsymbol{\varrho}_1, \boldsymbol{\varrho}_2 \rangle\!\rangle = \boldsymbol{\varrho}_1^T \boldsymbol{\varrho}_2$$

• distance function: assume $\|\varrho_1\| = \|\varrho_2\|$

$$d(\boldsymbol{\varrho}_1, \boldsymbol{\varrho}_2) = \|\boldsymbol{\varrho}_1\|^2 - \langle\!\langle \boldsymbol{\varrho}_1, \boldsymbol{\varrho}_2 \rangle\!\rangle = \|\boldsymbol{\varrho}_1\|^2 - \boldsymbol{\varrho}_1^T \boldsymbol{\varrho}_2.$$

Two spin $\frac{1}{2}$: Ising model

free Hamiltonian
 o in the lab frame

$$H_f = \omega_{o,\alpha} \Lambda_{03} + \omega_{o,\beta} \Lambda_{30} + h^{33} \Lambda_{33}$$

- $\omega_{o,\alpha}, \ \omega_{o,\beta} =$ Larmor frequencies of the single spins (\simeq MHz)
- $h^{33} = \text{scalar coupling (} \simeq \text{hundreds of Hz)}$
- if spins are homonuclear (gyromagnetic ratios $\gamma_{\alpha} = \gamma_{\beta}$) $\implies \omega_{o,\alpha}$ and $\omega_{o,\beta}$ differ only because of the chemical shift
- O if spins are heteronuclear: difference between $\omega_{o,\alpha}$ and $\omega_{o,\beta}$ can be of many MHz

Two spin $\frac{1}{2}$: Ising model

• control Hamiltonian

- 1. when $\omega_{o,\alpha} \simeq \omega_{o,\beta} \Longrightarrow$ spins are not selectively excitable: r.f. field resonating with $\omega_{o,\alpha}$ will cross-talk with the other spin \Longrightarrow one single control field
- 2. when difference between $\omega_{o,\alpha}$ and $\omega_{o,\beta}$ is high \Longrightarrow spins are selectively excitable \Longrightarrow 2 distinct control fields tuned at $\omega_{o,\alpha}$ and $\omega_{o,\beta}$
 - o in the lab frame

$$H_{\rm rf} = -B_1 \left(\cos(\omega_{\rm rf} t + \phi) \left(\gamma_\alpha \Lambda_{10} + \gamma_\beta \Lambda_{01} \right) + \sin(\omega_{\rm rf} t + \phi) \left(\gamma_\alpha \Lambda_{20} + \gamma_\beta \Lambda_{02} \right) \right)$$

• In the rotating frame, with $\phi = 0$

$$H_{\rm c} = -B_1 \left(\gamma_{\alpha} \Lambda_{10} + \gamma_{\beta} \Lambda_{01} \right)$$

Two spin $\frac{1}{2}$: Ising model

Case 1: nonselective control

• in a "single" rotating frame

$$H_{\rm f} = h^{03} \Lambda_{03} + h^{30} \Lambda_{30} + h^{33} \Lambda_{33}$$
$$H_{\rm c} = u \left(\Lambda_{01} + \Lambda_{10} \right)$$

•
$$h^{30} = -(\omega_{o,\alpha} - \omega_{rf}), \quad h^{03} = -(\omega_{o,\beta} - \omega_{rf})$$

• $u = -\gamma_{\alpha}B_1 = -\gamma_{\beta}B_1$

Case 2: selective control

• in a "doubly rotating" frame

$$H_{\rm f} = h^{03} \Lambda_{03} + h^{30} \Lambda_{30} + h^{33} \Lambda_{33}$$
$$H_{\rm c} = u_{01} \Lambda_{01} + u_{10} \Lambda_{10}$$

•
$$h^{30} = -(\omega_{o,\alpha} - \omega_{\mathrm{rf},\alpha}), \quad h^{03} = -(\omega_{o,\beta} - \omega_{\mathrm{rf},\beta})$$

• $u_{10} = -\gamma_{\alpha}B_{1,\alpha}, \quad u_{01} = -\gamma_{\beta}B_{1,\beta}$

Two spin $\frac{1}{2}$: Lie algebra structure

• "local" Lie algebra:

$$\mathfrak{su}(2) \oplus \mathfrak{su}(2) = \operatorname{span}\{-i\Lambda_{j0}, -i\Lambda_{0k}\}$$

• "nonlocal" Lie algebra:

$$\mathfrak{su}(2) \otimes \mathfrak{su}(2) = \operatorname{span}\{-i\Lambda_{jk}, j, k \neq 0\}$$

• "total" Lie algebra:

 $\mathfrak{g}_{2s} = \operatorname{Lie}\{-i\Lambda_{jk}, j, k = 0, \dots, 3\} = \mathfrak{su}(2) \oplus \mathfrak{su}(2) \cup \mathfrak{su}(2) \otimes \mathfrak{su}(2)$

• $\dim(\mathfrak{g}_{2s}) = 3 + 3 + 9 = 15$

case 1: nonselective control

- intuitively:
 - nonselective case: control field is the same for both spins
 - **O** coupling is only of the "z-z" type \implies symmetric
 - o in order to have controllability I need to "break the symmetry" by means of the local Larmor precessions
 - $\mathbf{O} \Longrightarrow$ there must be some chemical shift $h^{03} \neq h^{30}$
- Lie algebraic rank condition (LARC): if $\operatorname{Lie}\{-iH_{\mathrm{f}}, -iH_{\mathrm{c}}\} = \mathfrak{su}(2) \oplus \mathfrak{su}(2) \cup \mathfrak{su}(2) \otimes \mathfrak{su}(2) \implies$ the system $\dot{\rho} = -i[H_{\mathrm{f}} + uH_{\mathrm{c}}, \rho]$ is controllable
- controllability depends on the rotating frame chosen: consequence of the lack of small-time controllability
- check the LARC means compute exhaustively all the commutators $[-iH_f, -iH_c]$, $[-iH_f, [-iH_f, -iH_c]]$, $[-iH_f, -iH_c]$]
- long procedure also for 2 spin systems
- last time: sufficient condition for controllability in terms of energy levels

• free Hamiltonian

$$H_{f} = \begin{bmatrix} h^{03} + h^{30} + h^{33} & & \\ & -h^{03} + h^{30} - h^{33} & \\ & & h^{03} - h^{30} - h^{33} & \\ & & -h^{03} - h^{30} + h^{33} \end{bmatrix}$$

• control Hamiltonian

$$H_c = \begin{bmatrix} 0 & 1 & 1 & 0 \\ 1 & 0 & 0 & 1 \\ 1 & 0 & 0 & 1 \\ 0 & 1 & 1 & 0 \end{bmatrix}$$

• H_c is enabling the following transitions

$$1 \longleftrightarrow 2, \quad 1 \longleftrightarrow 3, \quad 2 \longleftrightarrow 4, \quad 3 \longleftrightarrow 4$$

• \Longrightarrow Graph (H_c) is connected

• sufficient condition for controllability: H_f is H_c strongly regular, meaning • energy levels of H_f are nondegenerate

 ${\rm O}$ energy levels of H_f are not equispaced along the transitions enabled by H_c

i.e.,
$$\begin{cases} h^{03} \neq h^{30} \\ h^{33} \neq \pm (h^{03} - h^{30})/2 \end{cases}$$

- when $h^{03} = h^{30}$, H_f has a degenerate energy level (of multiplicity 2)
- $\bullet \Longrightarrow$ sufficient conditions for controllability do not apply
- $\bullet \Longrightarrow$ system may be noncontrollable

case 2: selective control

- 2 control degrees of freedom u_{01} and u_{10}
- \implies LARC is always verified
- \implies the system

$$\dot{\rho} = -i[H_{\rm f} + u_{01}\Lambda_{01} + u_{10}\Lambda_{10}, \ \rho]$$

is always controllable

• you also have small time controllability \implies possibility to "kill" the drift

• commutator of $A_1 \otimes A_2$ and $B_1 \otimes B_2$

$$[A_1 \otimes A_2, \ B_1 \otimes B_2] = \frac{1}{2} \Big([A_1, \ B_1] \otimes \{A_2, \ B_2\} + \{A_1, \ B_1\} \otimes [A_2, \ B_2] \Big)$$

commutator for basis elements

$$[\Lambda_{jk}, \Lambda_{lm}] = \frac{1}{2} \left([\lambda_j, \lambda_l] \otimes \{\lambda_k, \lambda_m\} + \{\lambda_j, \lambda_l\} \otimes [\lambda_k, \lambda_m] \right)$$

• want to write it as "linear" operator

$$[\Lambda_{jk}, \Lambda_{lm}] = \mathrm{ad}_{\Lambda_{jk}} \Lambda_{lm}$$

 need to compute the structure constants (both symmetric and skew-symmetric ones)

• skew-symmetric structure constants

$$[\lambda_j, \lambda_k] = \operatorname{ad}_{\lambda_j} \lambda_k = \sum_{l=0}^3 c_{jk}^l \lambda_l$$

• symmetric structure constants

$$\{\lambda_j, \lambda_k\} = \operatorname{aad}_{\lambda_j} \lambda_k = \sum_{l=0}^3 s_{jk}^l \lambda_l$$

$aad_{\lambda_0} =$	[1	0	0	0		0	1	0	0
	0	1	0	0	$aad_{\lambda_1} =$	1	0	0	0
	0	0	1	0,	aau_{λ_1} –	0	0 0	0	0
	0	0 0	0	1		0	0	0	0
	Γο	0	1	0]		Γο	0	0	17
	0	0	1	0	-	0	0	0	1
anda —	0 0	0	1	0	- anda —	0 0	0	0	1
$aad_{\lambda_2} =$		0 0 0	1 0 0	$\begin{array}{c} 0\\ 0\\ 0\\ \end{array}$,	$\operatorname{aad}_{\lambda_3} =$		0 0 0	0 0 0	1 0 0

• Lie bracket

$$\begin{split} \left[\Lambda_{jk}, \Lambda_{lm}\right] &= \frac{1}{2} \left(\left[\lambda_j, \lambda_l\right] \otimes \left\{\lambda_k, \lambda_m\right\} + \left\{\lambda_j, \lambda_l\right\} \otimes \left[\lambda_k, \lambda_m\right] \right) \\ &= \frac{1}{2} \left(\operatorname{ad}_{\lambda_j} \lambda_l \otimes \operatorname{aad}_{\lambda_k} \lambda_m + \operatorname{aad}_{\lambda_j} \lambda_l \otimes \operatorname{ad}_{\lambda_k} \lambda_m \right) \\ &= \frac{1}{2} \left(\operatorname{ad}_{\lambda_j} \otimes \operatorname{aad}_{\lambda_k} + \operatorname{aad}_{\lambda_j} \otimes \operatorname{ad}_{\lambda_k} \right) \lambda_l \otimes \lambda_m \\ &= \operatorname{ad}_{\Lambda_{jk}} \Lambda_{lm} \end{split}$$

• adjoint operators $\operatorname{ad}_{\Lambda_{jk}} \longrightarrow$ infinitesimal superoperators

$$\operatorname{ad}_{\Lambda_{jk}} = \frac{1}{2} \left(\operatorname{ad}_{\lambda_j} \otimes \operatorname{aad}_{\lambda_k} + \operatorname{aad}_{\lambda_j} \otimes \operatorname{ad}_{\lambda_k} \right)$$

• 16×16 skew-symmetric matrices

Two spin $\frac{1}{2}$: Lie algebra of "unitary" superoperators

• "local" adjoint Lie algebra

 $\mathrm{ad}_{\mathfrak{su}(2)} \oplus \mathrm{ad}_{\mathfrak{su}(2)} = \mathfrak{so}(3) \oplus \mathfrak{so}(3) = \mathrm{span}\{-i\mathrm{ad}_{\Lambda_{j0}}, -i\mathrm{ad}_{\Lambda_{0k}}\}$

• "nonlocal" adjoint Lie algebra

 $\mathrm{ad}_{\mathfrak{su}(2)}\otimes\mathrm{ad}_{\mathfrak{su}(2)}=\mathfrak{so}(3)\otimes\mathfrak{so}(3)=\mathrm{span}\{-i\mathrm{ad}_{\Lambda_{jk}},\,j,k\neq 0\}$

• "total" Lie algebra:

 $\operatorname{ad}_{\mathfrak{g}_{2s}} = \operatorname{Lie}\{-i\operatorname{ad}_{\Lambda_{jk}}, j, k = 0, \dots, 3\} = \mathfrak{so}(3) \oplus \mathfrak{so}(3) \cup \mathfrak{so}(3) \otimes \mathfrak{so}(3)$

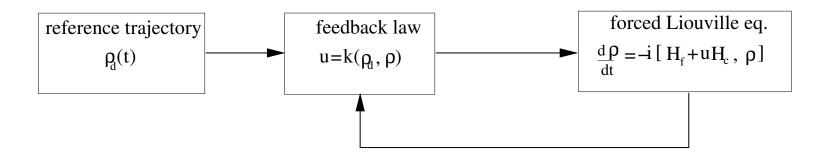
• $\dim(\mathrm{ad}_{g_{2s}}) = 3 + 3 + 9 = 15$

State feedback stabilization

Assumptions: state feedback stabilization problem:

- the entire state ρ is available on-line
- nonselective case: only one control degree of freedom
- desired state to track ρ_d is a pseudopure state
- ρ and ρ_d have the same eigenvalues

Scheme:



Feedback problem formulation

- given "reference density" $\rho_d(t)$
- "reference evolution" given by H_{f_d}

$$\dot{\boldsymbol{\varrho}}_d = -i \mathrm{ad}_{H_{f_d}} \boldsymbol{\varrho}_d$$

• want that the "true" evolution

$$\dot{\boldsymbol{\varrho}} = -i \left(\operatorname{ad}_{H_f} + u \operatorname{ad}_{H_c} \right) \boldsymbol{\varrho}$$

tracks the reference state determined by $\rho_d(t)$

$$\varrho \xrightarrow{t \to \infty} \varrho_d$$

o full state stabilization

Jurdjevic-Quinn sufficient condition for stabilization

- given a bilinear control system, if the so-called "ad-brackets" generate the entire Lie algebra, then ∃ a Lyapunov based feedback design → global stabilization
- automatically answers the problem of convergence (LaSalle invariance principle)
- it is never the case for manifolds with nontrivial topology

 $\operatorname{span}\left\{-i\operatorname{ad}_{H_f}, -i\operatorname{ad}_{H_c}, \left[-i\operatorname{ad}_{H_f}, -i\operatorname{ad}_{H_c}\right], \left[-i\operatorname{ad}_{H_f}, \left[-i\operatorname{ad}_{H_f}, -i\operatorname{ad}_{H_c}\right]\right], \dots, \right\} \neq \operatorname{ad}_{H_c}\right\}$

- to show it: compute the first commutators and verify that the basis directions $-i\Lambda_{11}$, $-i\Lambda_{12}$, $-i\Lambda_{21}$ and $-i\Lambda_{22}$ are never touched by such commutators
- stabilization design cannot be global!
- ullet \longrightarrow nontrivial singular locus
- $\bullet \longrightarrow$ in general: difficult to find what is the region of attraction

Proposition When $h^{03} \neq h^{30}$ and $H_{f_d} = H_f$, the feedback law

$$u = k \langle\!\langle \boldsymbol{\varrho}_d, -i \operatorname{ad}_{H_c} \boldsymbol{\varrho} \rangle\!\rangle, \qquad k > 0$$

asymptotically stabilizes the system

$$\dot{\boldsymbol{\varrho}} = -i \left(\operatorname{ad}_{H_f} + u \operatorname{ad}_{H_c} \right) \boldsymbol{\varrho}$$

to the reference state $\rho_d(t)$ for all $\rho(0)$ except for the following initial conditions

- 1. antipodal point of the reduced densities $(\boldsymbol{\varrho}_A(0), \, \boldsymbol{\varrho}_B(0)) = -(\boldsymbol{\varrho}_{A_d}(0), \, \boldsymbol{\varrho}_{B_d}(0))$
- 2. horizontal great circles of the reduced densities $(\varrho_A^3, \varrho_{A_d}^3) = (0, 0)$ and $(\varrho_B^3, \varrho_{B_d}^3) = (0, 0)$
- singular locus is the "replica" of the 1 spin 1/2 case
- k = feedback gain = parameter to tune

Sketch of the proof

• take Lyapunov function as before

$$V(t) = \left\| \boldsymbol{\varrho}_d \right\|^2 - \left\langle \left\langle \boldsymbol{\varrho}_d(t), \, \boldsymbol{\varrho}(t) \right\rangle \right\rangle > 0$$

- differentiate V
- $H_{f_d} = H_f \implies \text{drift disappears}$

•
$$\dot{V} = -u \langle\!\langle \boldsymbol{\varrho}_d, -i \operatorname{ad}_{H_c} \boldsymbol{\varrho} \rangle\!\rangle$$

- with $u = k \langle\!\langle \boldsymbol{\varrho}_d, -i \operatorname{ad}_{H_c} \boldsymbol{\varrho} \rangle\!\rangle \implies \dot{V} = -k \langle\!\langle \boldsymbol{\varrho}_d, -i \operatorname{ad}_{H_c} \boldsymbol{\varrho} \rangle\!\rangle^2 \leqslant 0$
- LaSalle invariance principle: want to find closed-loop trajectories that are in $\mathcal{N} = \{ \varrho \text{ s.t. } \dot{V} = 0 \}$
- $h^{03} \neq h^{30}$
 - $\mathbf{O} \implies$ local dynamics must be distinguishable
 - $\mathbf{O} \implies u = 0$ cannot belong to \mathcal{N} , except for the singular points

Jurdjevic-Quinn sufficient condition for stabilization

meaning of the Jurdjevic-Quinn condition:
 o take the linearization around the reference trajectory ρ_d

 $\dot{\boldsymbol{\varrho}} = -i \operatorname{ad}_{H_f} \boldsymbol{\varrho} + b u \qquad b = -i \operatorname{ad}_{H_c} \boldsymbol{\varrho}_d$

 \circ linearization lives on the tangent plane of $arrho_d$

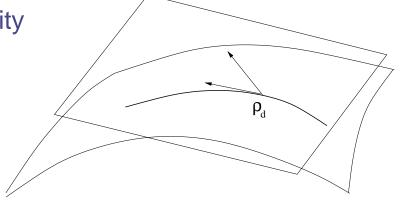
• if linearization satisfies the Kalman controllability condition

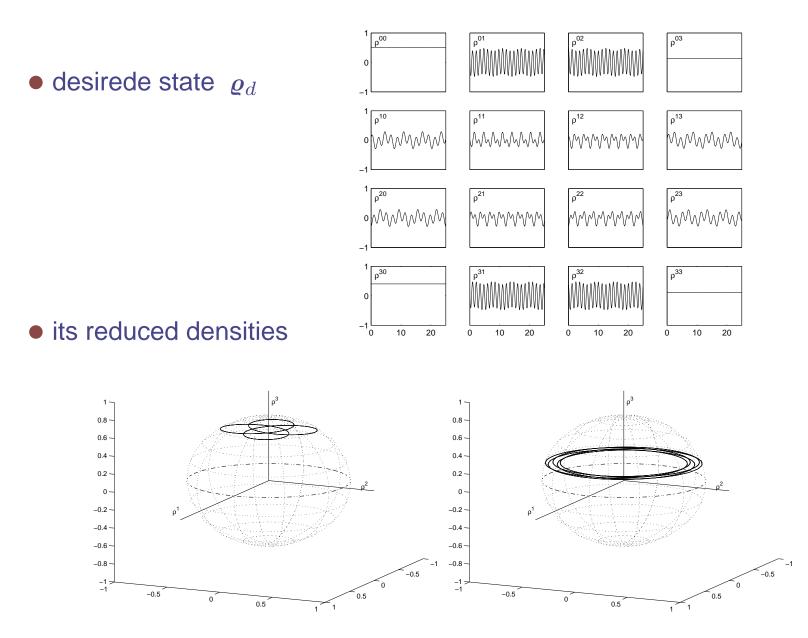
$$\operatorname{rank}\left[b - i\operatorname{ad}_{H_f} b \left(-i\operatorname{ad}_{H_f}\right)^2 b \dots\right] = \dim(\mathcal{S})$$

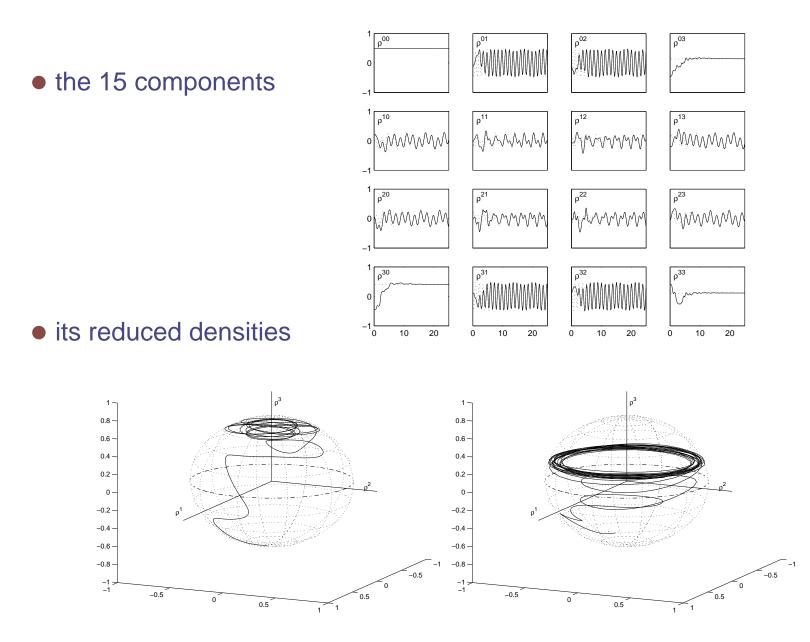
then there is no "direction" in which you can move the closed loop system while staying in $\mathcal{N}\Longrightarrow\mathcal{N}$ is empty

o ad-bracket ⇐⇒ Kalman controllability

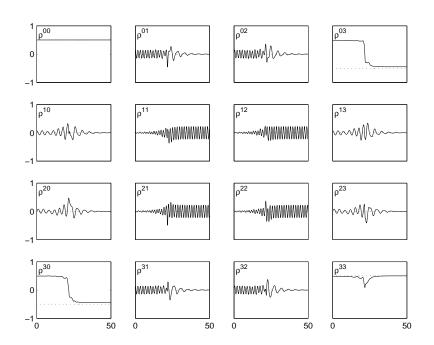
 when topology is nontrivial: linearization does not give global answers, only local







- presence of singularities
 - o "theoretically" state-to-state trasfer may fail
 - "practically" state-to-state transfer may be slow around the singular points (control action has to "build up" from 0)
- example $|00\rangle \rightarrow |11\rangle$
- it is better to apply an open-loop pulse to get approximately near the target and only then switch on the feedback



Generalizations

- 1. selective controls: tracking is easier since there are more control degrees of freedom
- 2. same theorem holds for n coupled spin 1/2
- 3. tracking Hamiltonians with any coupling

$$H_f \longrightarrow H_f = \sum_{jk} h^{jk} \Lambda_{jk}$$

• example: Heisenberg or dipole-dipole Hamiltonian

$$H_f = h^{03}\Lambda_{03} + h^{30}\Lambda_{30} + h^{11}\Lambda_{11} + h^{22}\Lambda_{22} + h^{33}\Lambda_{33}$$

- any other transversal term can be added as well, also $h^{jk}\Lambda_{jk}$, $j \neq k$
- prerequisite: controllability
- 4. only caveat: need to use $H_{f_d} = H_f$ in the theorem. Next: want to relax this constraint

• so far:
$$H_{f_d} = H_f$$

• \implies the derivative of the Lyapunov function is homogeneous in u

$$\dot{V} = -u \langle\!\langle \boldsymbol{\varrho}_{\mathrm{d}}, -i \mathrm{ad}_{H_c} \boldsymbol{\varrho} \rangle\!\rangle$$

ullet \Longrightarrow design of the feedback is "natural"

$$u = k \langle\!\langle \boldsymbol{\varrho}_{\mathrm{d}}, -i \mathrm{ad}_{H_c} \boldsymbol{\varrho} \rangle\!\rangle$$

and guarantees at least $\dot{V} \leqslant 0$.

• if $H_{f_d} \neq H_f$ then feedback design is more difficult, since \dot{V} is no longer homogeneous in u:

$$\dot{V} = \underbrace{\langle\!\langle \boldsymbol{\varrho}_{\mathrm{d}}, -i \mathrm{ad}_{(H_{f_d} - H_f)} \boldsymbol{\varrho} \rangle\!\rangle}_{\text{sign indefi nite term}} - u \langle\!\langle \boldsymbol{\varrho}_{\mathrm{d}}, -i \mathrm{ad}_{H_c} \boldsymbol{\varrho} \rangle\!\rangle$$

• want to see whether the algorithm is still converging

• call $H_{\delta} = H_{f_d} - H_f$ • H_{δ} = unwanted Hamiltonian • \longrightarrow disturbance to reject

• example:

 \circ H_{f_d} Ising Hamiltonian

$$H_{f_d} = h^{03}\Lambda_{03} + h^{30}\Lambda_{30} + h^{33}\Lambda_{33}$$

O H_f Heisenberg Hamiltonian or dipole-dipole Hamiltonian

$$H_f = h^{03}\Lambda_{03} + h^{30}\Lambda_{30} + h^{11}\Lambda_{11} + h^{22}\Lambda_{22} + h^{33}\Lambda_{33}$$

 $oldsymbol{O} \Longrightarrow H_{\delta}$ contains only transversal couplings $H_{\delta} = h^{11} \Lambda_{11} + h^{22} \Lambda_{22}$

Proposition If H_{δ} contains only "slow" couplings (approximately of one order of magnitude smaller than those of H_{f_d}) then \exists a sufficiently high feedback gain k and a ω_{rf} such that $\dot{\varrho} = -i(\operatorname{ad}_{H_f} + u\operatorname{ad}_{H_c})\varrho$ with the (nonselective) feedback controller $u = \langle\!\langle \varrho_d, -i\operatorname{ad}_{H_c} \varrho\rangle\!\rangle$ tracks the reference trajectory $\dot{\varrho}_d = -i\operatorname{ad}_{H_{f_d}} \varrho_d$

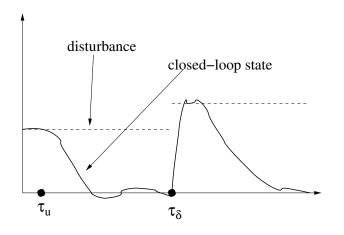
- H_{δ} is a "persistent" disturbance \longrightarrow never vanish
 - $o \Longrightarrow$ you never reach a steady state because of the persistent excitation
 - $o \Longrightarrow$ stability is only up to a small error \longrightarrow *practical stability*
- meaning of the Proposition: if H_{δ} is slow with respect to the feedback dynamics then it may not destroy convergence

Sketch of the proof

derivative of the Lyapunov function

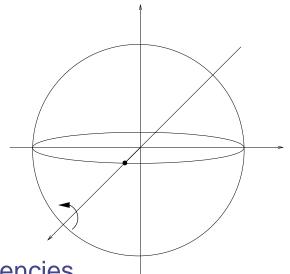
$$\dot{V} = \underbrace{\langle\!\langle \boldsymbol{\varrho}_{\mathrm{d}}, -i \mathrm{ad}_{(H_{f_d} - H_f)} \boldsymbol{\varrho} \rangle\!\rangle}_{\text{slow time scale } \tau_{\delta}} - \underbrace{u \langle\!\langle \boldsymbol{\varrho}_{\mathrm{d}}, -i \mathrm{ad}_{H_c} \boldsymbol{\varrho} \rangle\!\rangle}_{\text{fast time scale } \tau_u}$$

- in the fast time scale τ_u : disturbance can be thought as frozen
- ullet \Longrightarrow in the closed-loop dynamics it amounts to a constant "displacement"
- if the feedback can recover fast from such a displacement then convergence still holds



- Problem: control is along the λ_1 axis \implies when reduced density is aligned with λ_1 axis you have no control action
- $\bullet \Longrightarrow$ singularity of the control law

you need to get away from this alignement
by means of the coupling
by means of the local precession

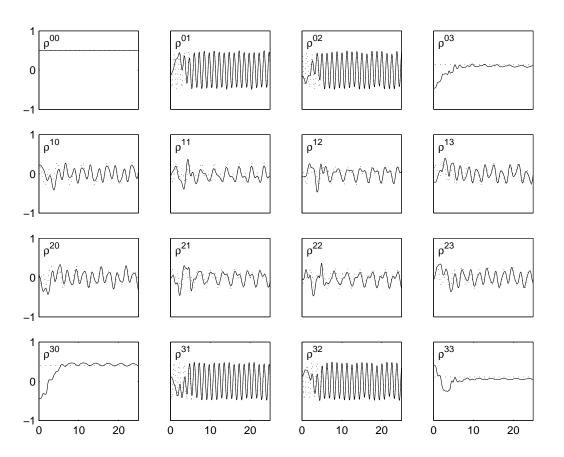


• to do it fast: choose ω_{rf} so that the Larmor frequencies

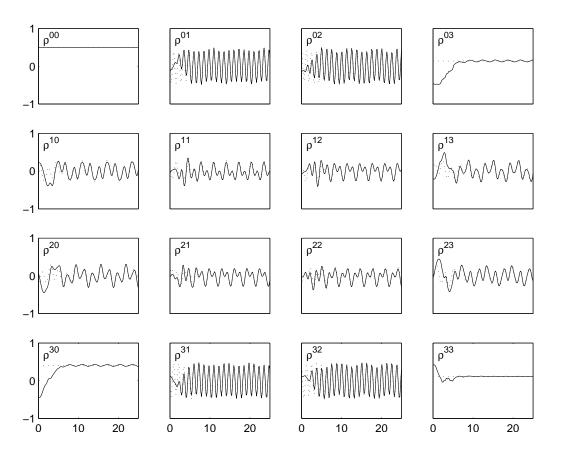
 $h^{30} = -(\omega_{0,\alpha} - \omega_{rf})$ and $h^{03} = -(\omega_{0,\beta} - \omega_{rf})$ are in the fast time scale

- \implies feedback loop
 - o exits fast from the singularities
 - \circ can recover the disturbance H_{δ} in the fast time scale
- feedback does not work for H_{δ} of the same order as H_{f_d}

- example mentioned above:
- H_{f_d} lsing, H_f Heisenbeg
- $H_{\delta} = h^{11}\Lambda_{11} + h^{22}\Lambda_{22}$



- if the controls are selective, then any coupling can be suppressed
- previous example: slow coupling



Suppression of unwanted couplings

- selective controls
- example: fast coupling to reject

$$\begin{array}{c} \bullet H_{\delta} = h^{11}\Lambda_{11} + h^{22}\Lambda_{22} \\ \bullet \tau_{\delta} \simeq \tau_{u} \\ & & & \\ & & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & & \\ & & \\ & & \\ & & & \\ & & \\ & & & \\ & & \\ & & & \\ & & \\ &$$

Suppression of unwanted couplings

- selective controls
- choosing two rf frequencies slightly off-resonance helps convergence
- same example:

• $H_{\delta} = h^{11}\Lambda_{11} + h^{22}\Lambda_{22}$ **O** $h^{03} = h^{30} = 0$ ρ⁰⁰ ρ⁰¹ M0 -1 ρ¹⁰ ρ¹¹ AMMM $\Lambda / \Lambda / \Lambda$ -1 $I \rho^{\overline{20}}$ 1 ρ³⁰ ρ³¹ \mathcal{M} MMM 0 -1 0 10 20 0 10 20 0 10 20 0 10 20

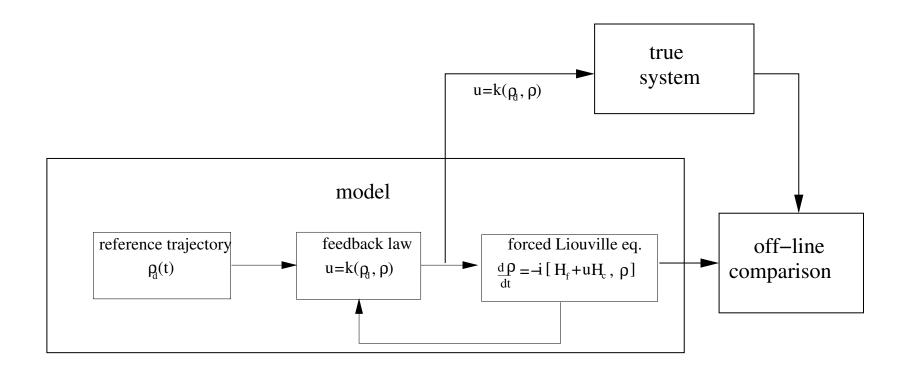
Using the algorithm for open loop control

- full state is *not* available \implies impossible to implement for real
- use scheme in an open-loop fashion, to generate time-dependent shaped pulses mapping $\varrho \longrightarrow \varrho_d$
- standard open-loop control methods
 - 1. hard pulses • high power \implies shorter times
 - 2. soft, shaped pulses \circ low power \implies long times
 - o both need selectivity
 - **O** simultaneous selective pulses \implies cross talk \implies need to precalculate the corrections
 - In presence of complicated couplings (solid state), both methods are difficult to use (remember: open-loop methods are "NP-hard")
- Is it possible to let the simulator compute the pulses by means of the "feedback on the model"?

Using the algorithm for open loop control

• open-loop control based on *feedback on the model* can be used for

- 1. "one-shot" gate (more properly: state transfer map)
- 2. "learn" from the simulator the control inputs that decouple an unwanted Hamiltonian

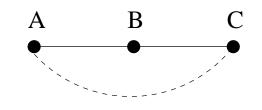


Using the algorithm for open loop control

- have the "true" state of the simulator track the desired reference, take the time-dependent control signal produced by the simulator and go to the lab.
- improvement w.r.t. the previous simulations: at t = 0 ρ can start already on the desired ρ_d
 - $\mathbf{O} \longrightarrow$ no need to "show asymptotic stability"
 - $o \longrightarrow no$ "transient" behavior
- \bullet prerequisite: need to known the initial condition \longrightarrow always the case in NMR
- any time you change the initial condition u(t) is different (simulator and feedback algorithms remain the same)
- drawback: profile of u(t) is normally not "nice"

aim: suppress unwanted couplings

- three identical spins, no chemical shift
- free Hamiltonian: dipole-dipole coupling
 - 1. two couplings between A-B and B-C



$$(-\Lambda_{110} - \Lambda_{220} + 2\Lambda_{330}) + (-\Lambda_{011} - \Lambda_{022} + 2\Lambda_{033})$$

2. one coupling (of weak strength) that I want to suppress between A-C

$$\frac{1}{8} \left(-\Lambda_{101} - \Lambda_{202} + 2\Lambda_{303} \right)$$

• control Hamiltonian: nonselective control field

$$u_1(\Lambda_{001} + \Lambda_{010} + \Lambda_{100})$$

• "disturbance" Hamiltonian

$$H_{\delta} = H_{f_d} - H_f = \frac{1}{8} \left(-\Lambda_{101} - \Lambda_{202} + 2\Lambda_{303} \right)$$

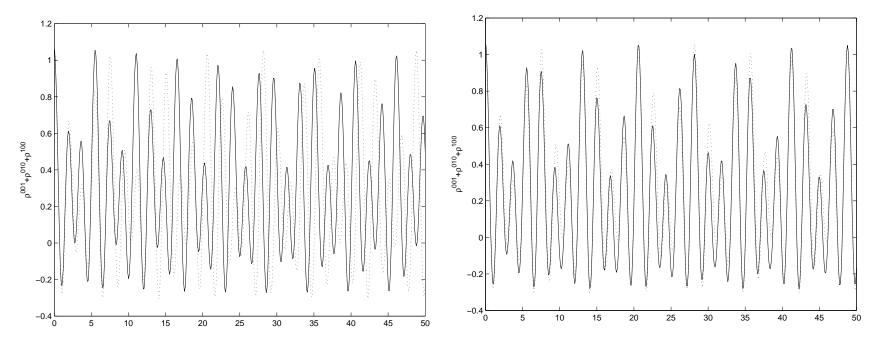
• initial state along the λ_1 axis

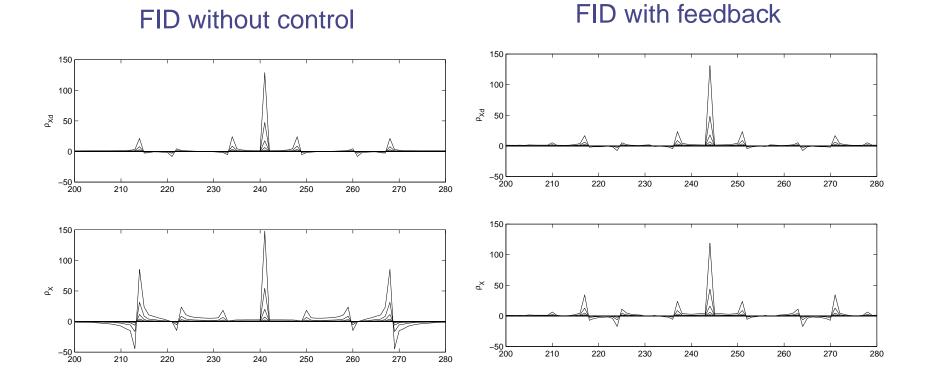
$$\boldsymbol{\varrho}(0) = \frac{1}{(\sqrt{2})^3} \begin{bmatrix} 1\\1\\0\\0 \end{bmatrix} \otimes \begin{bmatrix} 1\\1\\0\\0 \end{bmatrix} \otimes \begin{bmatrix} 1\\1\\0\\0 \end{bmatrix}$$

• look at the FID of the signal $\rho^{001} + \rho^{010} + \rho^{100}$

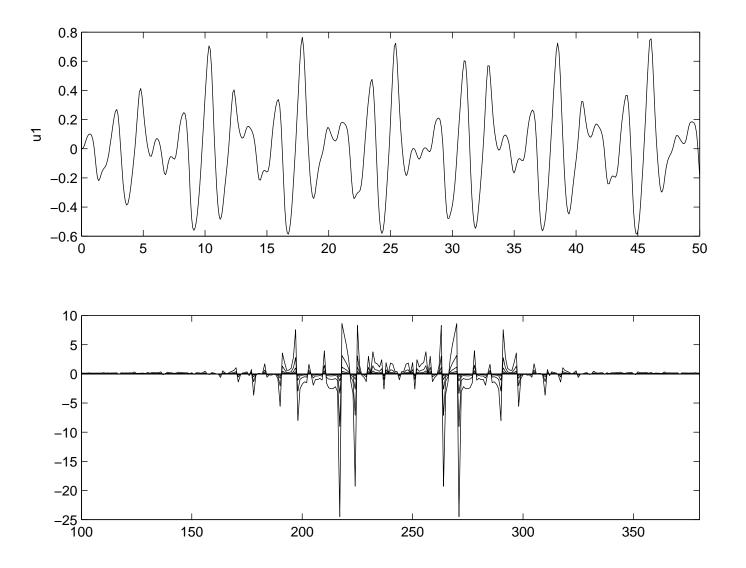
FID without control

FID with feedback

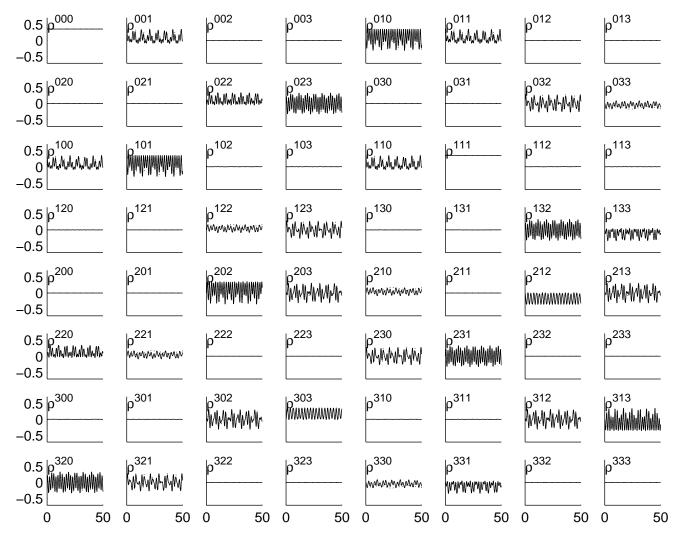




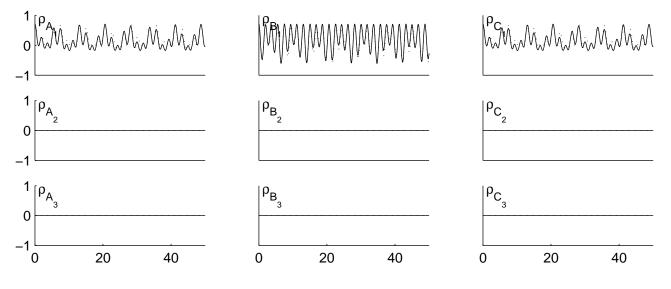
• control signal that does it

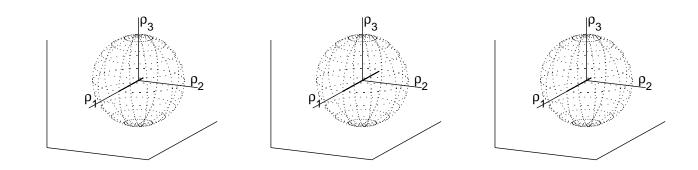


 how about the rest of the state? The feedback is decoupling the entire state space!

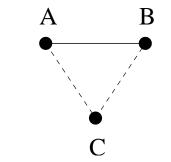


• for the 3 reduced densities





- three identical spins, no chemical shift
- free Hamiltonian: dipole-dipole coupling
 - 1. a couplings between A-B



$$\left(-\Lambda_{110} - \Lambda_{220} + 2\Lambda_{330}\right)$$

2. two couplings (of weak strength) that I want to suppress between A-C and B-C

$$+\frac{1}{8}\left(-\Lambda_{011} - \Lambda_{022} + 2\Lambda_{033}\right) + \frac{1}{8}\left(-\Lambda_{101} - \Lambda_{202} + 2\Lambda_{303}\right)$$

 \implies I want to decouple C from A-B

control Hamiltonian: nonselective control field

 $u_1(\Lambda_{001} + \Lambda_{010} + \Lambda_{100})$

• "disturbance" Hamiltonian

$$H_{\delta} = H_{f_d} - H_f = \frac{1}{8} \left(-\Lambda_{101} - \Lambda_{202} + 2\Lambda_{303} \right) + \frac{1}{8} \left(-\Lambda_{011} - \Lambda_{022} + 2\Lambda_{033} \right)$$

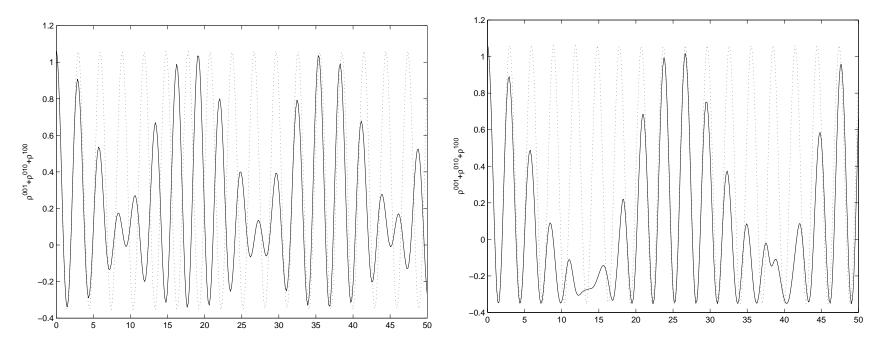
• initial state along the λ_1 axis

$$\boldsymbol{\varrho}(0) = \frac{1}{(\sqrt{2})^3} \begin{bmatrix} 1\\1\\0\\0 \end{bmatrix} \otimes \begin{bmatrix} 1\\1\\0\\0 \end{bmatrix} \otimes \begin{bmatrix} 1\\1\\0\\0 \end{bmatrix}$$

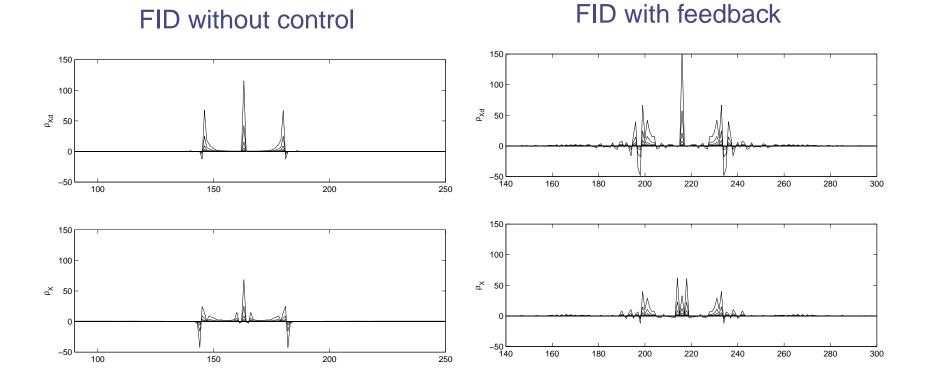
• look at the FID of the signal $\rho^{001} + \rho^{010} + \rho^{100}$

FID without control

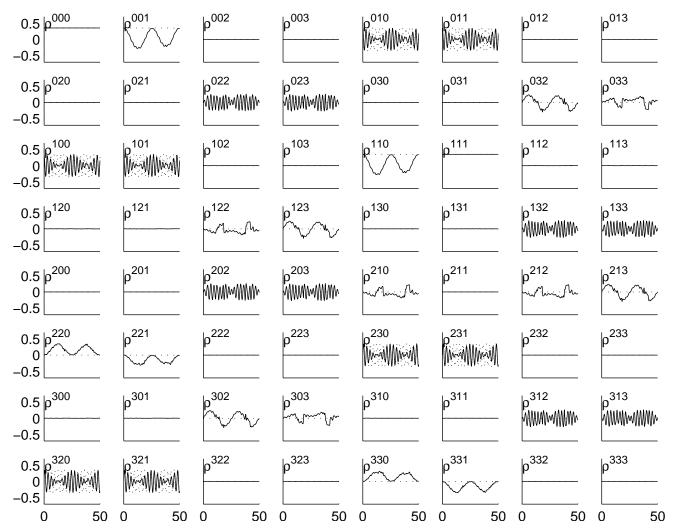
FID with feedback



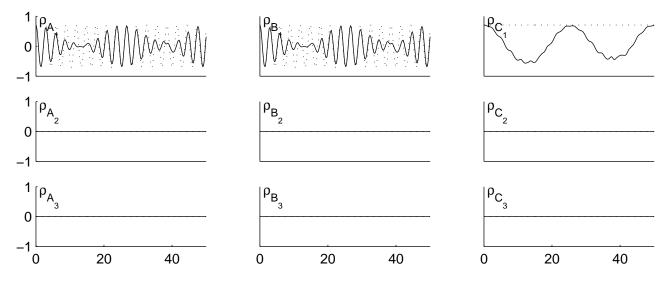
decoupling is not very good

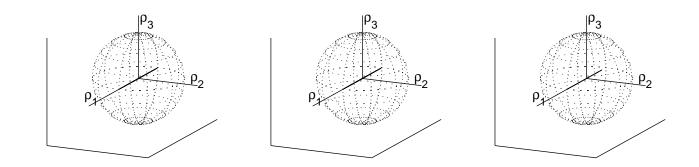


rest of the state



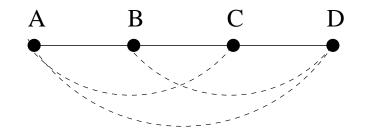
• for the 3 reduced densities

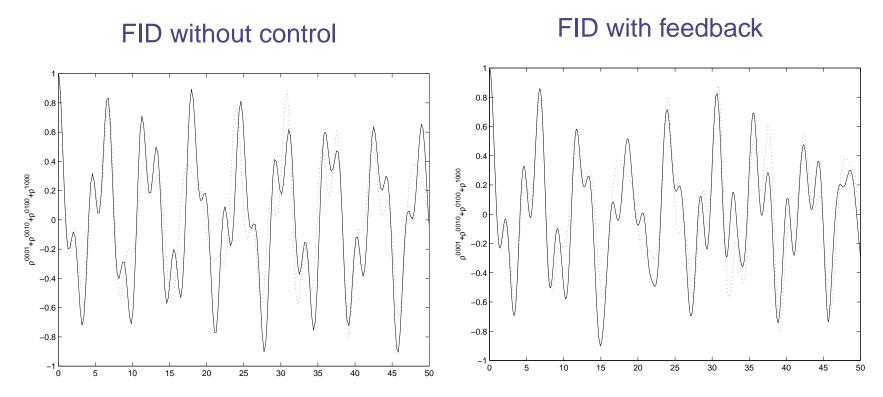




- 4 identical spins, no chemical shift
- free Hamiltonian: dipole-dipole coupling
 - 1. a couplings between A-B, B-C, C-D
 - 2. couplings to reject: A-C, B-D and A-D
 - 3. \implies want to make a linear spin chain
- control Hamiltonian: nonselective control field

 $u_1(\Lambda_{0001} + \Lambda_{0010} + \Lambda_{0100} + \Lambda_{1000})$



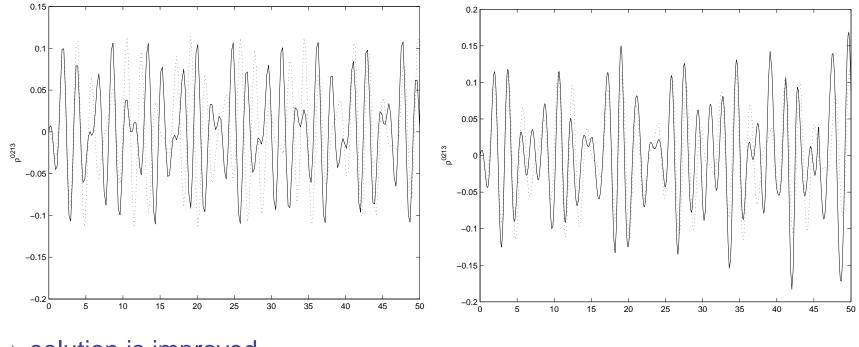


entire state space is already decoupled? Not really....

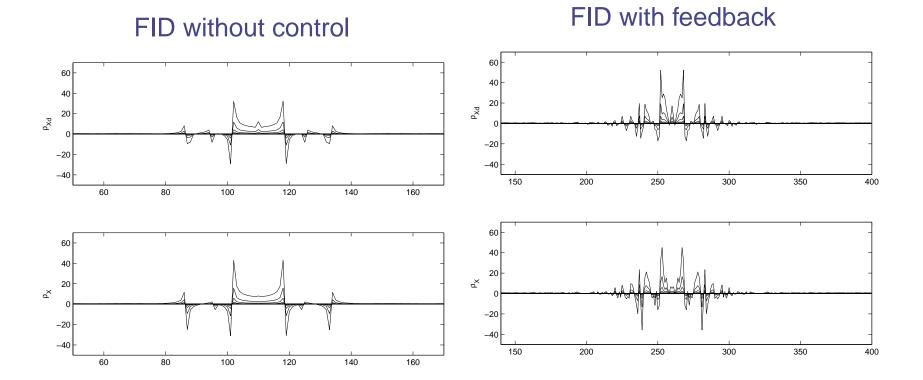


ρ^{0213} without control

ϱ^{0213} with feedback

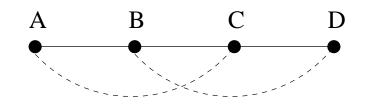


 \implies solution is improved



- 4 identical spins, no chemical shift
- free Hamiltonian: dipole-dipole coupling
 - 1. a couplings between A-B, B-C, C-D
 - 2. couplings to reject: A-C and B-D
 - 3. \implies want to make a linear spin chain
- control Hamiltonian: nonselective control field

 $u_1(\Lambda_{0001} + \Lambda_{0010} + \Lambda_{0100} + \Lambda_{1000})$



FID without control

FID with feedback

